Anoxic incubation of sediment in gas-tight plastic bags: a method for biogeochemical process studies

Jens Würgler Hansen*, Bo Thamdrup**, Bo Barker Jørgensen***

ABSTRACT: Incubation of sediment in gas-tight plastic bags is described as a method for experimental studies of biogeochemical processes. Sediment incubation in these bags allows time-course experiments to be conducted on homogenised sediment without dilution, continuous stirring, or gaseous head-space. Consequently, bag incubations of sediment combine the advantage of low heterogeneity in slurry incubations with the more natural conditions in jar and whole-core incubations. The bag material is a transparent laminated plastic comprised of Nylon, ethylenevinyl alcohol, and polyethylene with a low permeability for the studied gases: $O_2$, $CO_2$, $H_2$S, $CH_4$, $N_2$, $H_2$, and He. Estimated fluxes of biologically active gases through the plastic bag during sediment incubation were insignificant compared to rates of microbial processes and to gas concentrations in coastal sediments. An exception was $CH_4$, for which process calculations should include a correction for the exchange of $CH_4$ during incubation. Sulphate reduction rates measured in intact sediment cores and in sediment sectioned and incubated in the bags showed similar profiles in 3 coastal sediments with oxygen penetrations from a few millimetres to ~1 cm. In the most reduced sediment, whole-core and bag-based depth-integrated rates were the same while bag-rates exceeded whole-core rates by 1.4- and 3.2-fold in the intermediate and the most oxidised sediment, respectively. The differences may be related to the interruption of the biomediated transport of oxidants and the decay of fauna in the bag incubations.

KEY WORDS: Sediment incubation · Plastic bag · Gas-tight · Anoxic · Sulphate reduction

INTRODUCTION

Experimental sediment incubations, during which chemical concentrations and microbial populations are monitored over time, are often used in biogeochemical studies of anaerobic processes (e.g. Aller & Yingst 1980, Elsgaard & Jørgensen 1992). These time-course experiments have mainly been performed as either whole-core, jar or slurry incubations. Whole-core incubations of intact sediment have the advantage of minimal physical disturbance of the sediment. However, the quality of information obtained from whole-core incubations is limited by sediment heterogeneity, as the variation between replicate cores can be relatively high. Furthermore, the depth resolution of processes is in many instances poor, and it is not possible to make addition of substrates and inhibitor with uniform distribution in the sediment during whole-core incubation. Aller & Mackin (1989) have described 2 methods that are useful for studies of rates in undisturbed sediments based on changes in concentrations of solutes. One of the methods is an alternative incubation system (plug incubation), whereby the surface of a sediment slice is exposed to a well-stirred water reservoir, while the other method is the more traditional whole-core
incubation. These systems have the advantage of maintaining natural zonations in the sediment, but they require incubation periods of at least 1 wk and imply knowledge of reaction orders and diffusion constants.

Sediment typically has to be homogenised to obtain reproducible results in the short-time incubations that are necessary to maintain the original rates, pathways, and microbial populations. In jar incubations, a portion of initially homogenised sediment is distributed into sealed containers which are sacrificed at different time points (e.g. Aller & Yingst 1980, Fossing & Jorgensen 1990, Kristensen et al. 1999). However, the heterogeneity between the individual containers is higher than in incubations where sampling is done from a continuously mixed portion of sediment.

In slurry incubations, addition of water to the sediment enables continuous stirring and mixing during incubation. However, the dilution of the porewater and the physical agitation may significantly affect the processes under investigation (Jørgensen 1978, Bak et al. 1990, Kristensen et al. 1999). Furthermore, slurries have often been incubated in bottles in which the ratio of slurry to gas phase decreases over time as a consequence of sampling. This changes the concentration in the slurry of dissolved gases in equilibrium with the head-space. The loss of gases from the slurry is especially problematic if the head-space is exchanged during the incubation, e.g. by flushing with nitrogen.

Consequently, there is a need for alternative methods for the experimental study of microbial and geochemical processes in sediments. We evaluate here the use of gas-tight plastic bags as a method for incubation of anoxic sediment. The method is discussed in relation to the above-mentioned approaches. The permeability of a multi-laminar plastic film to oxygen (O₂), carbon dioxide (CO₂), hydrogen sulphide (H₂S), methane (CH₄), dinitrogen (N₂), hydrogen (H₂), and helium (He) is presented, and the permeability of the biologically active gases during sediment incubations is evaluated in relation to key anaerobic processes. We also evaluate the effect of sediment homogenisation in bag incubations on anaerobic mineralisation.

**MATERIALS AND METHODS**

Theory. The permeation of molecules through a membrane can be divided into 2 steps: (1) solution of the permeant in the membrane, and (2) diffusion of the dissolved permeant. Permeability (P) can be expressed as the product of the solubility coefficient (S) and the diffusion constant (D) (Rogers et al. 1956, Crank 1975, Pauly 1989):

\[ P = S \times D \] (1)

The permeability depends on the nature of the membrane, the nature of the permeant, and the interaction between the membrane and the permeant. The value of D and thereby P generally increases with humidity and temperature (Rogers et al. 1956).

The permeability of a film to a gas is defined by the flux (F) of the gas through the film multiplied by the thickness (x) of the film and divided by the difference in partial pressure (Δp) over the film (Crank 1975):

\[ P = \frac{F \times x}{\Delta p} \] (2)

The flux is the amount of gas (n) passing through a membrane per area (A) and per time (t):

\[ F = \frac{n}{A \times t} \] (3)

By combining Eqs. (2) & (3), P can be expressed as:

\[ P = \frac{n \times x}{A \times t \times \Delta p} \] (4)

**Multi-laminar plastic film.** Bags for anoxic incubations of sediment were made from a 180 µm-thick transparent laminated plastic (NEN/PE 80/100, Danisco Flexible, Denmark: Fig. 1A). The laminate consists of 4 layers with the following properties: (1) Nylon, which is of high mechanical strength (outer layer), (2) ethylenevinyl alcohol (EVOH), which is extremely impermeable to gases, (3) Nylon, a second strengthening layer, and (4) polyethylene, which seals easily and is a good water barrier (inner layer). NEN/PE is a non-toxic material, free of plasticizers, and is mainly used for vacuum-packaging of fresh meat.

Bags, 30 cm × 30 cm in size, were produced from a single sheet of plastic by the use of an impulse heat-sealer (Elwis-Pack, Andertech International, Denmark). The plastic bags were mounted with a glass outlet via a screw cap and 2 gaskets (Fig. 1B). The opening in the outlet was sealed with a rubber stopper.

**Fluxes of specific gases.** Experiments were performed at room temperature (ca 22°C) and a relative humidity of 30 to 60%.

The flux of O₂ into a bag filled with 1.9 l of autoclaved, anoxic artificial seawater (28‰) was determined by monitoring the O₂ concentration for a period of 102 d. The bag was pasteurised after 48 and 82 d (heated to 70°C for 0.5 h). The O₂ concentration was determined in duplicate by the Winkler method (Strickland & Parsons 1972, p. 21–26), modified to measure low O₂ concentrations in small volumes. Samples of 5 ml were withdrawn through the stopper in the outlet using a glass syringe with a 3-way stopcock. Immediately before sampling, the syringe and the stopcock were flushed with N₂. Winkler reagents (0.04 ml each) and concentrated phosphoric acid (0.08 ml) were
added to the sample in the syringe through a butyl rubber stopper mounted in the stopcock. Sampling was only accepted if the difference between duplicates was <2.5 µM. The measured concentrations were corrected for the O2 content in the reagent according to Carpenter (1965).

The flux of H2S was determined in 2 bags filled with 2.0 l autoclaved, anoxic artificial seawater (sulphate-free, phosphate buffered, pH 7.8, 28‰) enriched with 264 µM $\sum H_2S (= H_2S(aq) + HS^- + S^{2-})$. At pH 7.8, the concentration of $H_2S(aq)$ is 18 µM, corresponding to 7% $\sum H_2S$ (Morse et al. 1987). The $\sum H_2S$ concentration of the artificial seawater was followed for 73 d. The bags were stored in an anoxic glove box with an atmosphere of 95% nitrogen and 5% hydrogen. Samples of 4 ml were withdrawn with a syringe through the stopper in the outlet. The samples were fixed in 1 ml of 5% zinc acetate before removal from the glove box. The $\sum H_2S$ concentration was determined spectrophotometrically according to Cline (1969).

Fluxes of CO2 and H2 were determined in 3 parallel bags filled with 2.3 to 2.7 l pure CO2 or H2 gas and incubated for 39 d. The plastic material was allowed to equilibrate with the respective gases for 2 d before the final filling. The fluxes of CO2 and H2 were estimated from the decrease in the bag volume corrected for the diffusion of O2 and N2 into the bags. The bag volume was determined from the rise in water level upon submersion of the bag. Similarly, the flux of He was determined in a single bag filled with 3.4 l of pure He, which was incubated for 36 d. The concentrations of O2 and N2 in the bags were analysed at the beginning and at the end of the experiment using a gas chromatograph equipped with a flame ionization detector (Packard). Separation was done on a Poropak Q column.

Fluxes of the tested gases were determined from the best linear fit to the change in concentration or volume with time. The flux of O2 into the bag containing water were estimated both after the 1st and 2nd pasteurisation. The fluxes of O2 and H2S were corrected for the water removed at each sampling, but were not corrected for the loss of water vapour during incubations since this accounted for only a small percentage of the total volume.

**Mixing efficiency of sediment in plastic bags.** Silty sediment was sampled at 16 m water depth at Stn 6, Aarhus Bay, Denmark (see following subsection). The sediment was transferred to a plastic bag and homogenised without dilution by manual kneading of the bag. A time-course experiment was run to test the efficiency of this homogenisation procedure. A few microlitres of $^{35}SO_4^{2-}$ were injected into 0.8 l sediment and the bag was kneaded for 15 min. During the first 10 min, 2 g of sediment were sampled through the outlet every minute followed by sampling after 12 and 15 min. Afterwards the bag was cut open and a sample was collected from each corner. The samples were mixed with 10 ml of water, centrifuged, and 5 ml of the supernatant were mixed with 5 ml scintillation liquid and counted in a scintillation counter (Tri-Carb 2200 CA, Packard).

**Sulphate reduction in bag and whole-core incubations.** Sediment profiles of sulphate reduction obtained in bag and whole-core incubations were compared for 3 sediments. Sediment was collected at 2 sites in Aarhus Bay, Denmark in July, 1995. Stn 6, at 16 m depth in the middle of the bay, had a silty sediment which graded from brown and oxidised at the surface to black at ~6 cm depth, below which hydrogen sulphide accumulated in the porewater. The station is described in detail by Thamdrup et al. (1994) and Jørgensen (1996). The other station was situated at 10 m depth inside the small inlet Knebel Vig. This sediment consisted of a fine-grained black sulphidic mud covered by an ~0.5 cm oxidised surface layer. There was no evidence of infauna in this reduced sediment. The third station was situated at 36 m depth in the fjord Young Sound in Northeast Greenland. The station is described in detail by Rysgaard et al. (1998).
Sediment from the 2 sites in Aarhus Bay was sampled with a box corer and sub-sampled into 9.6 and 2.8 cm i.d. Plexiglas liners for bag and whole-core incubations, respectively. The cores were sampled from the same box cores and care was taken to keep sediment for the 2 types of incubation under the same conditions. Sulphate reduction rates were determined by the radiotracer technique using a tracer solution of 40 kBq µl⁻¹ carrier-free $^{35}$SO$_4^{2-}$ (Jørgensen 1978). For bag incubations, sediment from 6 large cores was sectioned, homogenised, and loaded into bags anoxically as described by Canfield et al. (1993b) and Thamdrup & Canfield (1996). The bags were incubated at in situ temperature (8°C) inside a larger N$_2$-filled bag. After about 1 d incubation, ~8 cm$^3$ of sediment from each bag was loaded anoxically into 10 ml syringes with the tips cut off. A volume of 8 µl tracer was injected and the syringes were closed with rubber stoppers. In parallel, 2 small sediment cores were injected with 5 µl tracer through silicon-sealed ports at 1 cm depth intervals. The resultant activity for both bag and core incubations was ~40 kBq cm⁻³ sediment. Syringes and cores were incubated at 8°C for 4 h, and the incubations were terminated by extruding the sediment from the syringes and sectioning the whole-cores into 10 ml of 20% (w/w) zinc acetate solution. Quantification of radiolabelled reduced sulfur, analysis of sulphate concentration, and calculation of sulphate reduction rates were carried out according to Fossing & Jørgensen (1989). Sediment from Young Sound was sampled and handled similarly, as described in detail by Rysgaard et al. (1998).

**RESULTS AND DISCUSSION**

**Flux and permeability of gases**

Fluxes of gases through the NEN/PE film were determined from changes in concentration (O$_2$, H$_2$S and N$_2$) and volume (CO$_2$, H$_2$, and He) in the bags (Fig. 2).

The bag containing autoclaved artificial seawater had to be pasteurised before the O$_2$ concentration increased. The linear increase in the O$_2$ concentration after the first and second pasteurisation corresponded to an O$_2$ flux into the bag of 5.0 ± 0.3 (SE) µmol m$^{-2}$ d$^{-1}$ (Fig. 2A, Table 1). The low steady O$_2$ concentration during the first 48 d of incubation was due to O$_2$ consumption, which presumably was caused by contamination with aerobic bacteria from the inside of the non-sterilised plastic bag. A H$_2$S flux out of the bags of 1.5 ± 0.3 (SE) µmol m$^{-2}$ d$^{-1}$ was determined from the linear decrease in the ΣH$_2$S concentration in the 2 bags (Fig. 2B, Table 1). The drop in the ΣH$_2$S concentration within the first day was due to sorption of H$_2$S in the plastic film and oxidation of H$_2$S by the O$_2$ introduced during filling of the bags. Therefore, the start concentration was not included in the calculation of the flux. The decrease in volume of the bags containing CO$_2$, H$_2$, and He allowed us to calculate fluxes out of the bags of 980 ± 87 (SE, n = 3), 2078 ± 130 (SE, n = 3), and 12 068 (n = 1) µmol m$^{-2}$ d$^{-1}$, respectively (Fig. 2C, Table 1). The concurrent increase of the O$_2$ and N$_2$ concentration in the bags containing CO$_2$ and H$_2$ corresponded to fluxes of O$_2$ and N$_2$ into these bags of 56 ± 6 (SE, n = 6) and 86 ± 5 (SE, n = 3) µmol m$^{-2}$ d$^{-1}$, respectively (Table 1).
The fluxes of gases obtained in this and other studies were used to calculate the permeability of the plastic film to O₂, CO₂, H₂S, CH₄, N₂, H₂, and He (Table 1). Due to sorption of water in the outer Nylon layer, the permeability increases strongly with the outside humidity. Therefore, it is important to keep the bag dry on the outside to reduce the permeability to gases. In addition, permeability increases when temperature rises. Thus, the permeability of the NEN/PE film increases 6-fold at an increase in relative outside humidity from 58 to 99% and increases 4-fold at a temperature increase from 5 to 25°C (P. Togeskov pers. comm.). The dramatic effect of humidity is underlined by the 12-fold increase of the permeability to O₂ when a bag is surrounded by water instead of air (Table 1, see also Kruse 1993).

The permeability to O₂ was much lower when a bag contained water than when it contained gas, despite similar external humidity and temperature during the 2 tests. We have no explanation for this observation. The permeability of O₂ in water is about 4000 times higher than the permeability in the plastic film. Thus, the lower permeability in the bag with water cannot be caused by the diffusive boundary layer that establishes in the water as a thin film on the inside of the plastic bag. We presume that the permeabilities to CO₂, N₂, and H₂ would also have been lower if measured in bags containing water instead of gas. Therefore, the fluxes of these gases in sediment incubations are best estimated from the O₂ flux into the bag that contain water times the ratio of O₂ and the respective gas permeabilities obtained in the bags that contain gas (Table 2). The permeabilities to O₂ and CO₂ found in this study were significantly higher than the permeabilities measured by the manufacturer (Table 1). This was mainly due to a much lower outside humidity (5% relative humidity) during the tests done by the manufacturer (P. Togeskov pers. comm.). However, other experimental differences, such as the use of single sheets of plastic film instead of bags for the permeability test by the manufacturer may also have been of importance.

Table 1. Gas diffusion through bags made of plastic film NEN/PE 80/100. Bags contained 2 to 3 l of either water or gas, and had a surface area of 0.1 to 0.2 m². Positive and negative values indicate whether concentration is highest outside or inside bag (Gradient), concentration in bag increases or decreases (Conc. change), and whether flux is into or out of bag (Flux). Gradient is difference in partial pressure between inside and outside of plastic film; relative concentration change (Rel. change) shows by how much % equilibrium is approved per day under given starting conditions. Permeability: volume of gas (transformation from µmol to cm³) was calculated at temperature given in table. rh = relative humidity; nd = no data

<table>
<thead>
<tr>
<th>Gas</th>
<th>Content</th>
<th>Temperature T (°C)</th>
<th>Humidity (rh)</th>
<th>Gradient (bar)</th>
<th>Conc. change (µmol l⁻¹ d⁻¹)</th>
<th>Rel. change (% d⁻¹)</th>
<th>Flux (µmol m⁻² d⁻¹)</th>
<th>Permeability (cm⁻³ cm⁻³ m⁻² d⁻¹)</th>
<th>Source</th>
</tr>
</thead>
<tbody>
<tr>
<td>O₂</td>
<td>Water</td>
<td>22</td>
<td>30–60</td>
<td>0.21</td>
<td>0.21</td>
<td>0.23</td>
<td>5</td>
<td>10</td>
<td>This study</td>
</tr>
<tr>
<td>O₂</td>
<td>Water</td>
<td>10</td>
<td>nd, air</td>
<td>0.20</td>
<td>0.7</td>
<td>0.24</td>
<td>12a</td>
<td>25</td>
<td>Kruse (1993)</td>
</tr>
<tr>
<td>O₂</td>
<td>Water</td>
<td>10</td>
<td>100, water</td>
<td>0.18</td>
<td>7.4</td>
<td>2.51</td>
<td>123a</td>
<td>287</td>
<td>Kruse (1993)</td>
</tr>
<tr>
<td>H₂S</td>
<td>Water</td>
<td>22</td>
<td>nd, air</td>
<td>-0.0002b</td>
<td>-0.2</td>
<td>0.06</td>
<td>-2</td>
<td>3671</td>
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<tr>
<td>CH₄</td>
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<td>22</td>
<td>nd, air</td>
<td>-0.68</td>
<td>-8.2c</td>
<td>0.91</td>
<td>-134c</td>
<td>87</td>
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<td>Gas</td>
<td>22</td>
<td>30–60</td>
<td>0.21</td>
<td>4.9</td>
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<td>56</td>
<td>118</td>
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<tr>
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<td>Gas</td>
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<td>5</td>
<td>1.00</td>
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<td>ndd</td>
<td>21</td>
<td>9</td>
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<tr>
<td>CO₂</td>
<td>Gas</td>
<td>22</td>
<td>30–60</td>
<td>-1.00</td>
<td>-90.7</td>
<td>0.22</td>
<td>-980</td>
<td>428</td>
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<tr>
<td>N₂</td>
<td>Gas</td>
<td>22</td>
<td>30–60</td>
<td>-1.00</td>
<td>-173.2</td>
<td>0.42</td>
<td>-2078</td>
<td>917</td>
<td>This study</td>
</tr>
<tr>
<td>He</td>
<td>Gas</td>
<td>22</td>
<td>30–60</td>
<td>-1.00</td>
<td>-701.6</td>
<td>1.70</td>
<td>-12068</td>
<td>5263</td>
<td>This study</td>
</tr>
</tbody>
</table>

aCalculated based on information from author of a bag volume of 3 l and a surface area of 0.2 m²
bMeasurements were made at pH 7.8, at which H₂S constitutes 7% of ∑H₂S
cCalculated based on information from authors of a bag volume of 2 l, a surface area of 0.1 m² and a CH₄ concentration of 0.9 mM
dAbsolute and relative concentration change could not be calculated, as a sheet of plastic was used instead of a bag in measurements of permeability by the manufacturer

Table 2. Ratio of gas permeabilities compared to permeability of O₂ for plastic film NEN/PE (80/100): based on data from Table 1

<table>
<thead>
<tr>
<th>Gases</th>
<th>Content</th>
<th>Ratio</th>
</tr>
</thead>
<tbody>
<tr>
<td>H₂S:O₂</td>
<td>Water</td>
<td>367</td>
</tr>
<tr>
<td>He:O₂</td>
<td>Gas</td>
<td>45</td>
</tr>
<tr>
<td>CH₄:O₂</td>
<td>Water</td>
<td>9</td>
</tr>
<tr>
<td>H₂:O₂</td>
<td>Gas</td>
<td>8</td>
</tr>
<tr>
<td>CO₂:O₂</td>
<td>Gas</td>
<td>4</td>
</tr>
<tr>
<td>N₂:O₂</td>
<td>Gas</td>
<td>4.4</td>
</tr>
<tr>
<td>N₂:O₂</td>
<td>Gas</td>
<td>0.4</td>
</tr>
</tbody>
</table>

aData from this study
bData from this study and Hansen et al. (1998)
cData from manufacturer
The sequence for the permeabilities of gases for NEN/PE was: H$_2$S > He > CH$_4$ > H$_2$ > CO$_2$ > O$_2$ > N$_2$, with the permeability of H$_2$S being ~900 times higher than the permeability of N$_2$. Permeabilities calculated from fluxes into and out of the bags can be compared, as permeability is not significantly dependent on the direction of the flux (P. Togeskov pers. comm.). The permeabilities and their sequence depend on the composition of the plastic and, therefore, vary between different films. However, the sequence of permeabilities in plastic films is generally in the order (H$_2$S, He, H$_2$, and CO$_2$) > O$_2$ > N$_2$ (Rogers et al. 1956, Pauly 1989).

The applicability of NEN/PE bags to anoxic incubation of sediment is demonstrated by the following comparison of measured bag fluxes of biologically active gases and rates of microbial processes in sediment. From the literature we adopted gross rates of key microbial processes and porewater concentrations from relevant biogeochemical zones of coastal marine sediments (Table 3). We assumed that 2000 cm$^3$ of sediment contained in a gas-tight plastic bag with a surface area of 0.2 m$^2$ was incubated in air, and we calculated the flux into or out of the bag based on the permeabilities of the plastic film. The permeabilities to CO$_2$, N$_2$, and H$_2$ were estimated as the permeability to O$_2$ obtained with water in the bag multiplied with the respective factors from Table 2, as discussed above. The flux of O$_2$ into the bag could cause an aerobic carbon oxidation corresponding to 0.2% of the carbon oxidation by sulphate reduction. The introduced O$_2$ might also be consumed by oxidation of H$_2$S, which would correspond to oxidation of 0.2% of the H$_2$S produced by sulphate reduction. Furthermore, the diffusive loss of H$_2$S would be <1% of its production rate, and similarly <1% of the production rates of CO$_2$, N$_2$, and H$_2$ would be lost by diffusion out of the bag (Table 3). The loss of CH$_4$ was estimated as 11% of its production rate. Consequently, rates of CH$_4$ cycling obtained from sediment incubations in bags should be corrected for the loss of CH$_4$ during incubation. The higher loss of CH$_4$ than the other gases was due to a combination of a relatively high permeability of the plastic film to CH$_4$ and a large gradient across the plastic barrier.

The above calculations of the relative gas loss during bag incubation are based on one combination of concentration and production rate for each gas (Table 3). However, in typical sediments a higher or lower production rate will be found in combination with a higher or lower concentration, respectively. As a result these different combinations of concentrations and rates will not significantly change the calculated relative loss of gas. The listed process rates are from experiments at in situ temperature, whereas the permeabilities used for the above calculations are for room temperature; therefore, the relative losses are overestimated in the calculations.

Release of gases from or uptake of gases into the plastic film may also affect the measurements of microbial processes and concentrations during incubations in bags. The inside of the plastic film is made of polyethylene, which has an oxygen solubility comparable to water (Pauly 1989). If 2000 cm$^3$ of anoxic sediment were incubated in a bag with a surface area of 0.2 m$^2$, the volume of ethylene in the plastic would correspond to 1% of the sediment volume. Accordingly, the release of O$_2$ from the ethylene would have a minor initial effect on processes and concentrations in the sediment. Similarly, the sorption of H$_2$S, CO$_2$, CH$_4$, N$_2$, and H$_2$ into the plastic film would only slightly change their respective concentrations in the sediment. Furthermore, the exchange of gases will happen rapidly compared to the duration of most incubations, as equilibrium between the gases in the plastic film and the environment is attained within 1 h (Stern & Frisch 1981, P. Togeskov pers. comm.).

### Sediment incubations in bags compared to other methods

A plastic bag containing fine-grained sediment with tracer added was kneaded by hand, and the mixing

<table>
<thead>
<tr>
<th>Component</th>
<th>Conc. (µM)</th>
<th>Rate (nmol cm$^{-3}$ d$^{-1}$)</th>
<th>Loss (%)</th>
<th>Source</th>
</tr>
</thead>
<tbody>
<tr>
<td>O$_2$</td>
<td>300</td>
<td>10 000</td>
<td>0.2</td>
<td>Rasmussen &amp; Jørgensen (1992)</td>
</tr>
<tr>
<td>$\Sigma$CO$_2$</td>
<td>4000</td>
<td>400</td>
<td>0.002</td>
<td>Mackin &amp; Swider (1989)</td>
</tr>
<tr>
<td>$\Sigma$H$_2$S</td>
<td>50</td>
<td>100</td>
<td>0.03</td>
<td>Thamdrup et al. (1994)</td>
</tr>
<tr>
<td>N$_2$</td>
<td>450</td>
<td>50</td>
<td>0.5</td>
<td>Rysgaard &amp; Berg (1996)</td>
</tr>
<tr>
<td>CH$_4$</td>
<td>500</td>
<td>70</td>
<td>11</td>
<td>Hansen et al. (1994)</td>
</tr>
<tr>
<td>H$_2$</td>
<td>0.01</td>
<td>60</td>
<td>0.0001</td>
<td>Hoehler et al. (1994)</td>
</tr>
</tbody>
</table>

Table 3. Typical porewater concentrations and production rates in relevant biogeochemical zones of coastal sediments. Loss = calculated loss of gases during sediment incubation due to permeability of plastic bag in relation to production rates at a temperature of 22°C, salinity of 28%, and pH of 7.8. For data of CO$_2$ are from top few millimetres of sediment; loss represents maximal reduction of sulphate reduction rate due to permeability of O$_2$; See ‘Results’ for further details. $\Sigma$CO$_2$ = CO$_2$$_{(aq)}$ + H$_2$CO$_3$ + HCO$_3^–$ + CO$_3^{2–}$, $pk_3 = 1.25 \times 10^{-6}$, $pk_2 = 9.13 \times 10^{-10}$ (Millero 1995); $\Sigma$H$_2$S = H$_2$S$_{(aq)}$ + HS$^–$ + S$^{2–}$, $pk_1 = 2.16 \times 10^{-7}$ (Morse et al. 1987). H$_2$ production rate was assumed to equal H$_2$ consumption rate, which was calculated as 4 times the CO$_2$ reduction rate.
efficiency was monitored by measuring the radioactivity in sub-samples in a time series. The radioactivity in the sediment samples reached a stable level after 3 min of kneading, which demonstrates that the sediment in the bag was homogenised rapidly, even out into the corners (Fig. 3). Therefore, time-course experiments using bag incubations allow repeated sampling from a homogenised portion of sediment, which reduces the sediment heterogeneity compared to both whole-core and jar incubations. Consequently, shorter incubations are needed to detect changes in bag incubations than in whole-core or jar incubations. This lowers the risk of altering the microbial populations or their metabolic pathways. In addition, in bag incubations, the disturbance from addition of water and continuous mixing, as in slurry incubations, is avoided.

Anaerobic methane oxidation rates determined in bag incubations were similar to rates determined for intact sediment cores (Hansen et al. 1998), whereas anaerobic methane oxidation rates in sediment slurries can be several orders of magnitude lower than rates obtained for intact sediment cores (Alperin & Reeburgh 1985). The reason is presumably that syntrophic microbial associations such as inter-species hydrogen transfer are disturbed by continuous agitation (Dannenberg et al. 1997), a problem which is largely overcome in bag incubations.

The NEN/PE bags have been applied in many studies of anaerobic microbial processes in sediments and microbial mats (Canfield et al. 1993a,b, Hansen et al. 1993, Holmer & Kristensen 1994a,b, Thamdrup & Canfield 1996, Habicht & Canfield 1997, Hansen et al. 1998, Rysgaard et al. 1998, Kostka et al. 1999, Glud et al. 2000). NEN/PE bags have also been used as incubation systems for the study of plankton production and respiration, for the measurement of microbial processes in sewage, and for growing enrichment cultures (S. Rysgaard pers. comm., L. P. Nielsen pers. comm., K. Finster pers. comm.). A general agreement has been observed between rates of anaerobic microbial processes obtained in bag incubations and in intact sediment cores from the same location (Thamdrup & Canfield 1996, Hansen et al. 1998, Kostka et al. 1999). However, in some cases, rates obtained from bag incubations are higher than rates obtained for whole-cores (Canfield et al. 1993a, Thamdrup et al. 1996, Glud et al. 2000, Thamdrup & Canfield 2000). For a more precise evaluation of the effects of sediment disturbance during bag incubations on process rates, we compared sulphate reduction rates in intact sediment cores and bag incubated sediment. Sulphate reduction was chosen because it is often the most important anaerobic respiration in coastal sediments, and rates can be determined at high spatial resolution in intact cores (Jørgensen 1978, 1982). Care was taken to minimise the possible influence of spatial heterogeneity and difference in incubation temperature and time on rate determination.

In the Knebel Vig sediment there was good agreement between sulphate reduction rates obtained below 1 cm depth, while bag-based rates were consistently higher than whole-core rates at Stn 6 and in Young Sound (Fig. 4). The ratio of depth-integrated bag-based and whole-core sulphate reduction rates below the oxic zone was 1.1, 1.4, and 3.2 at Knebel Vig, Stn 6 and Young Sound, respectively. As the sulphate reduction rates obtained in bag and whole-core incubations approach each other with increasing depth in the sediment (Fig. 4), the ratio of depth-integrated bag-based and whole-core sulphate reduction rates will be less at deeper depth-integration. The increase in the ratio of depth-integrated bag-based and whole-core sulphate reduction rates from Knebel Vig, Stn 6 to Young Sound, was paralleled by decreasing sulphate reduction rates and less reduced porewaters. Thus, hydrogen sulphide was present below 1 cm depth at Knebel Vig while it appeared at ~5 cm depth at Stn 6 and was not detected in Young Sound (Thamdrup et al. 1994, Rysgaard et al. 1998, Thamdrup 2000).

Similar effects of sediment homogenisation have been observed in other studies: (1) Jørgensen (1978) found that sulphate reduction was enhanced if oxidised and reduced sediment were mixed, whereas homogenisation of reduced sediment did not stimulate sulphate reduction; (2) in a comparison of sulphate reduction rates obtained in jar and whole-core incubations of continental margin sediments, Kristensen et al. (1999) found that rates obtained in jar incubations were only enhanced in the upper few centimetres of
the sediment, which make up the most oxidised part; (3) Mackin & Swider (1989) found that in 2 very reduced sediments the integrated $\Sigma$CO$_2$ production from incubation of homogenised sediment agreed well with $\Sigma$CO$_2$ fluxes in core incubations.

The variable effect of homogenisation between sediment types and with sediment depth is presumably due to a combination of several factors: (1) homogenisation of sediment may remove or reduce inhibition of bacterial processes in substrate-rich microenvironments and may cause organic aggregates to become accessible to degradation (Glud et al. 2000); (2) rapid degradation of entombed fauna in incubation bags may stimulate anaerobic processes (Canfield et al. 1993a); (3) influx of oxidants through, e.g., bioturbation and bioirrigation is blocked in bag incubations, which may stimulate sulphate reduction. The 2 latter points would be more significant in oxidised sediments since these generally harbour more infauna than highly reduced sediments (Pearson & Rosenberg 1978). It should be noted that the cores we used to sample sediment for the bag incubations covered a much larger sediment area (72 cm$^2$) than the cores we used for the whole-core incubations (6 cm$^2$). Larger animals and their associated burrow structures are especially difficult to sample in the small cores used for whole-core incubations. Thus, if a particularly high microbial activity is associated with these animals, whole-core rates may underestimate sediment metabolism due to the exclusion of larger animals, whereas bag incubations may overestimate sediment metabolism due to degradation of entombed fauna.

**Choice of plastic material**

Because of their gas-barrier properties, plastic bags made of Tedlar (PVdC, polyvinylidene chloride), Saran (PVF, polyvinyl fluoride), and Transpak (glass-coated polypropylene or polyethylene) have been used to store gas samples and for packaging food (van Kessel 1983, Posner & Woodfin 1986, Modern Plastics International 1990). However, the permeability to O$_2$ in EVOH, the gas-tight layer in NEN/PE used in this study, is 3, 15, and 30 times lower than in Transpak, Saran, and Tedlar, respectively (Pauly 1989, Modern Plastics International 1990, Eriksen et al. 1993). Furthermore, our experience has shown that NEN/PE is a more robust material than both Tedlar and Saran. Plastic films with a thin laminate of aluminium foil are even more gas-tight than NEN/PE (Cragg et al. 1992, Kruse 1993, Carlson et al. 1999). Compared to NEN/PE, these aluminium foil films have the disadvantage of being opaque, which makes it difficult to check for and remove trapped gas pockets. Furthermore, the aluminium foil is not as robust as the NEN/PE film, as the aluminium tends to crack when manipulated, which increases the permeability of the aluminium foil.

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**Fig. 4.** Sulphate reduction rates (SRR) in sediments of Aarhus Bay, Denmark, and Young Sound, Greenland, obtained in bag and whole-core incubations. Dashed lines indicate oxygen penetration depths. Sulphate reduction measured in oxic zone is not presented for bag incubation, as oxic zone turned into anoxic zone during these incubations. Variation indicated by error bars is difference between 2 parallel measurements divided by 2. At Young Sound, bag incubation was done only once. Data from Young Sound have in part been presented by Rysgaard et al. (1998). Note different scales for sulphate reduction rates.
Practical advice

Sediment is transferred to the bag while it is still open on one side. The inside of the bag at the opening is carefully wiped clean before it is heat-sealed. Alternatively, the open side may be folded and closed with clamps. The permeability in bags closed with clamps has not been measured. Weldings on heat-sealed bags should be placed about 1 cm from the edge of the plastic film to make room for an extra welding should the first one fail during kneading or incubation. It is also advisable to make weldings across the corners to avoid blind pockets and to facilitate complete homogenisation of the sediment in the bag. Homogenisation of sediment in the bag is easier if a gas pocket of N₂ is included in the bag during kneading and afterwards removed through the outlet. The plastic film is heat-stable up to at least 80°C, but cannot be autoclaved without structural deformation (P. Togeskov pers. comm.). The opening of the outlet in the bag needs to have a minimum i.d. of 6 mm to allow sediment to pass through. A spout cut and welded directly as part of the plastic bag can replace the glass outlet. The spout is closed by a clamp after being folded. Sampling from a bag containing water or gas can be done with syringe and needle through an adhesive rubber membrane pasted onto the outside of the bag (e.g. a 2.5 mm-thick Melamine [EDPM, ethylene propylene terpolymer] membrane is suitable). The membrane closes the hole after the needle is removed. If the incubation is long or so sensitive to O₂ that even the low permeability of the NEN/PE film is problematic, the O₂ flux can be reduced many-fold by incubating the bag within a larger N₂-filled NEN/PE bag. Furthermore, the O₂ that fluxes into the larger N₂-filled bag can be removed completely by a chemical O₂ scrubber, which is commercially available in small sachets.

Conclusion

NEN/PE is an extremely gas-tight laminated plastic material, which is suitable for incubation of samples of gases, water and sediments. Except for CH₄, the fluxes of biologically active gases through the plastic film were insignificant compared to rates of microbial processes in the sediment. Rates of microbial processes in reduced sediments obtained in bag incubations generally agree well with rates obtained in whole-cores. However, in more oxidised sediments, anaerobic processes are overestimated in bag incubations, presumably due to a combination of factors such as removal of process inhibition, degradation of entombed fauna, and prevention of transport of oxidants.

Gas-tight plastic bags are in many ways superior to other types of containers used for sediment incubations. Their main advantages are: (1) the material is extremely gas-tight; (2) sediment can be homogenised without addition of water; (3) continuous stirring is not needed during time-course experiments; (4) sub-sampling can be done without introducing a gas phase; (5) bags and their content can be pasteurised as the plastic is heat-stable up to at least 80°C; (6) the material can be sterilised with acid, alcohol and hydrogen peroxide; (7) the material is very flexible and bags can be constructed in any size or shape; (8) the material is robust, transparent, light and inexpensive.

Gas-tight plastic materials are produced by companies selling packing materials to the food industry. The plastic material NEN/PE is produced in several versions with different thicknesses of the layers of Nylon and polyethylene, but with the same barrier properties as for NEN/PE 80/100 tested in this study, and is available from Danisco Flexible, Lyngby, Denmark.

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